





An atomistic investigation of the interaction of dislocations with Guinier-Preston zones in Al-Cu alloys

G. Esteban-Manzanares, E. Martinez, J. Segurado, J. Llorca



OUTLINE

A) Motivation

- 1 VIRMETAL PROJECT
- 2- Atomistic simulation and modeling of Al-Cu alloys
- 3 Al-4%Cu alloy precipitation sequence

B) Atomistic simulations of dislocation Guinier-Preston zones interaction

- 1 Atomistic Setup
- 2 Simulation methodology
- 3 Results

Transition state theory with direct Molecular Dynamics Nudged elastic band method Thermodynamics of Dislocation-GP zone Predictions of flow stress based on atomistic results

C) Conclusions



MOTIVATION

1 – VIRMETAL PROJECT

- Development a bottom- up multiscale strategy to design, process and test advances metallic alloys
- Six main tasks involved this project

<u>Connect atomistic-microscales</u>

- o Bridging microscale-macroscale
- o Multiscale modeling of plastic deformation and fracture
- Computational thermodynamics and kinetics
- \circ $\;$ Multiscale modeling of casting and solidification $\;$
- o Experimental validation
- Focused on <u>AI-Cu</u> and Mg-AI-Zn
- *Objective :* Provide information from classical atomistic approaches (MD, MC, NEB) to larger scale simulations.





- 2 ATOMISTIC SIMULATION AND MODELING OF AI-Cu ALLOYS
 - Investigate the interaction of different type of dislocations with precipitates.
 - o Overcome mechanisms
 - \circ $\,$ Critical resolved shear stress $\,$
 - Activation energies
 - o Thermodynamic study
 - Quantify how **solid solution affects** to the motion of dislocation
 - Compute the activation energies for other mechanisms of overcoming obstacles. i.e. Cross Slip in screw dislocations
 - **Development of models** to use in higher length scales i.e. Discrete Dislocation Dynamics



MOTIVATION

3 – AI-4%Cu ALLOY PRECIPITATION SEQUENCE

- Al4%Cu alloys presents a well-stablished sequence of precipitation
- Solid Solution \rightarrow <u>Guinier-Preston zones</u> $\rightarrow \theta'' \rightarrow \theta' \rightarrow \theta$
- Depending on the heat treatment, different precipitation will appear.
- Naturally aged Al-4%Cu (504 h at room temperature) alloy contains in mostly Guinier-Preston zones (GP).
- GP zones features:
 - Aggregates of Cu atoms
 - Mono layer disk shaped precipitates
 - {100} family of planes
 - Totally coherent precipitates
 - From 2-10 nm of diameter.









1 – ATOMISTIC SETUP

- The system contains around **1.38 million** of atoms
- Inserted an **edge dislocation** with Volterra's displacement field.
- GP zones show 2 different interaction angles as a function of Burgers vector of a dislocation in its slip plane: 60 degrees, 0 degrees
- Inserted **GP zone in the (100) plane**, which represent a 60 degree obstacle for the dislocation in the slip plane.
- The atomic setup try to **mimic** as close as possible the microstructure of **AI-4%Cu alloy** naturally aged.





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- 2 SIMULATIONS METHODOLOGY
- Activation enthalpy (ΔH) and activation Gibbs free energy (ΔG) of interaction between dislocation and GP60 zones a have been study by means of two different classical atomistic approaches:
 - Classical Molecular Dynamics simulations (MD) have been devoted to obtain the rate of the dislocation to overcome GP zone. Using transition state theory (TST) obtain the activation Gibbs free energy.



- NVT ensemble with Langevin thermostat and constant strain applied in the upper boundary.
- With a timestep of 2 fs wait until the dislocation overcome the GP zone.
- A range of temperatures from 400-600 K in steps of 50K and from 140 to 170 MPa in steps of 10 Mpa.
- 8 independent MD simulations for each couple of stress and temperature.



- 2 SIMULATIONS METHODOLOGY
- Activation enthalpy (ΔH) and activation Gibbs free energy (ΔG) of interaction between dislocation and GP60 zones a have been study by means of two different classical atomistic approaches:
 - The **nudged elastic band method (NEB)** has been utilized to compute the **activation enthalpy** as a function of the applied strain with 16 replicas.





3 – RESULTS

• Molecular dynamics simulations have provide the average rate for the dislocation to overcome the GP zone.

$$\frac{N}{\sum_{1}^{N} t_{MD}} = \overline{\Gamma} = v_0 exp\left(\frac{-\Delta G(\tau)}{k_b T}\right) \rightarrow v_0 = 4 - 5x10^{10} \frac{1}{s}$$

 Nudged Elastic band simulations gave the activation enthalpy profile as a function of the shear stress applied.





3 – RESULTS:

• Comparing the thermodynamic results obtained with both NEB and MD simulations.



• **Difference** between both results should come from the **entropic factor** $\Delta S(T, \tau)$.



3 – RESULTS:

- Up to the moment we have obtained
 - Δ*G* as a function of stress applied, but does not depend on temperature.
 - ΔH as a function of applied stress.
 - Activation volume V_a is constant with respect to the stress.

$$\frac{\partial \Delta G}{\partial \tau} = -\frac{\partial \Delta U}{\partial \tau} + V_a + T \frac{\partial \Delta S}{\partial \tau} \rightarrow \frac{\partial \Delta F}{\partial \tau} = 0 \rightarrow \frac{\partial \Delta U}{\partial \tau} = T \frac{\partial \Delta S}{\partial \tau}$$

• Variation of internal energy and variation of entropy should be parallel curves.

$$\Delta S = \frac{1}{T} \left(\Delta H - \Delta G \right) \quad \rightarrow \quad$$

$$\Delta S = \frac{1}{T} [(A - \Delta F) - (B - V_a)\tau]$$

• Finally using the the definition of activation Gibbs free energy is obtained

$$\Delta G = \Delta U - T \Delta S - \tau V_a \quad \rightarrow \quad$$

$$\Delta \boldsymbol{U} = [\boldsymbol{A} - (\boldsymbol{B} - \boldsymbol{V}_a)\boldsymbol{\tau}]$$



- 3 RESULTS:
- Entropic factor is a function of the temperature O(T⁻¹) and applied stress
- Variation of **internal energy** depends just on the **stress**. Activation Helmholtz free energy is the distance between both thermodynamic functions.



$$\Delta \boldsymbol{U} = [\boldsymbol{A} - (\boldsymbol{B} - \boldsymbol{V}_a)\boldsymbol{\tau}]$$

$$\Delta S = \frac{1}{T} [(A - \Delta F) - (B - V_a)\tau]$$

HTST to hold the entropic factor:

$$\Delta S = k_b \log\left(\frac{\prod_{i}^{N-1} \nu_i^{min}}{\prod_{i}^{N-1} \nu_i^{saddle}}\right)$$

• In the case studied, dependence of temperature of $\Delta S(T^{-1})$ suggest that HTST does not hold.



- 3 RESULTS:
- **Prediction of the thermal contribution of the flow stress** of Al-4%Cu naturally aged based on thermodynamic results and TST.



- The source of discrepancies might be:
 - Just GP60 zones and edge dislocation taken into account.
 - Athermal contribution of the flow stress.
 - Distribution of precipitates.



- Our simulations suggest that harmonic transition state theory does not hold to this phenomenon.
- A prediction of thermal contribution of the flow stress has been carried out, with the thermodynamic results obtained.
- Experiments proved more complex behavior than the one study here.







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THANK YOU FOR YOU ATTENTION